## A glimpse at Sampled-Data systems Nothing new, just some elements from literature

Pierre Vuillemin (ONERA / DTIS / COVNI)



#### Idea behind the research team COVNI:

+



computer theory



automatic control

=



something interesting for computer-controlled systems

- [1] Boyd and Barratt. Linear controller design: limits of performance. 1991
- [2] Chen and Francis. Optimal sampled-data control systems. 1995

Idea behind the research team COVNI:



computer theory



automatic control



something interesting for computer-controlled systems

- How do we assess dynamical performances of an implemented control-law?
  - give some insights concerning what "performance" may refer to for control people

=

- introduce some concepts from sampled-data systems theory
- talk restricted to Linear Time Invariant (LTI) models

<sup>[1]</sup> Boyd and Barratt. Linear controller design: limits of performance. 1991

<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

Idea behind the research team COVNI:



computer theory



automatic control



something interesting for computer-controlled systems

How do we assess dynamical performances of an implemented control-law?

- give some insights concerning what "performance" may refer to for control people
- introduce some concepts from sampled-data systems theory
- talk restricted to Linear Time Invariant (LTI) models

References:

- ▶ a comprehensive introduction to control engineering can be found in the first chapters  $(1 \rightarrow 3)$  of [1]
- what will be presented on sampled-data systems can be found in [2]

<sup>[1]</sup> Boyd and Barratt. Linear controller design: limits of performance. 1991

<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

# Outline

Performances of a controlled system

Quantifying discretization error

Continuous lifting and measure of performance for SD systems

Conclusion

# What is control engineering all about? I

In a nutshell

```
dynamical system + actuators/sensors + control objectives = control problem (1)
tracking, disturbance rejection, etc.
```

# What is control engineering all about? I

#### In a nutshell

```
dynamical system + actuators/sensors + control objectives = control problem (1)
tracking, disturbance rejection, etc.
```

#### And in practice ...?

Different philosophies: pole placement, loop-shaping, convex synthesis...

 $\hookrightarrow$  Here: focus on the approach relying on the specification of a performance function to be optimized  $\sim$  optimal feedback control

# What is control engineering all about? I

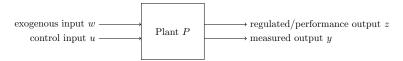
#### In a nutshell

```
dynamical system + actuators/sensors + control objectives = control problem (1)
tracking, disturbance rejection, etc.
```

#### And in practice ...?

Different philosophies: pole placement, loop-shaping, convex synthesis...

 $\hookrightarrow$  Here: focus on the approach relying on the specification of a performance function to be optimized  $\sim$  optimal feedback control



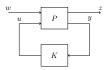
Modelling of the control problem = derive the generalized plant P:

- ▶ models for the dynamical system + actuators/sensors  $\rightarrow$  this sets u and y
- identify reference signals, possible disturbances or noise  $\rightarrow$  w
- select signals of interest for the control objective  $\rightarrow z$

# What is control engineering all about? II

### Standard form

The loop is closed with some controller K,

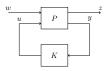


- most of the control architectures can be represented as this standard form,
- K can have different structures: a gain, PI, PID, etc.
- ▶ the closed-loop is the transfer from w to z, denoted  $T_{w \to z}(P, K)$ ,
- ▶ in general, one wants K to stabilize (internally) the plant P.

# What is control engineering all about? II

#### Standard form

The loop is closed with some controller K,



- most of the control architectures can be represented as this standard form,
- K can have different structures: a gain, PI, PID, etc.
- the closed-loop is the transfer from w to z, denoted  $T_{w \to z}(P, K)$ ,
- ▶ in general, one wants K to stabilize (internally) the plant P.

### **Optimal control**

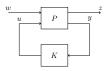
Find K that stabilizes P internally and minimizes  $||T_{W\to z}||$ 

For fixed plant *P*, performance of the closed-loop = value of  $||T_{w \to z}||$ 

# What is control engineering all about? II

#### Standard form

The loop is closed with some controller K,



- most of the control architectures can be represented as this standard form,
- K can have different structures: a gain, PI, PID, etc.
- the closed-loop is the transfer from w to z, denoted  $T_{w \to z}(P, K)$ ,
- ▶ in general, one wants K to stabilize (internally) the plant P.

### **Optimal control**

Find K that stabilizes P internally and minimizes  $||T_{W \to z}||$ 

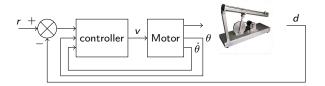
For fixed plant P, performance of the closed-loop = value of  $||T_{w \to z}||$ 

#### Linear-Time Invariant case

- ▶ practical interpretation of  $T_{w \to z}$  convenient in the frequency-domain (transfer function)
- ▶ useful systems norms:  $\mathcal{H}_{\infty}$ ,  $\mathcal{H}_{2}$

## What is control engineering all about? III

A tracking example: ball on the beam

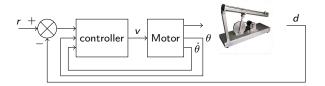


Physical modelling

- dynamical sytem: beam + ball,
- actuator: motor e.g. controlled by a voltage  $v \rightarrow u$
- ▶ sensed signals: the distance *d* of the ball to the center of the beam, the angular position  $\theta$  and velocity  $\dot{\theta}$  of the shaft of the motor  $\rightarrow y = [r d, \theta, \dot{\theta}]^T$

## What is control engineering all about? III

A tracking example: ball on the beam



Physical modelling

- dynamical sytem: beam + ball,
- actuator: motor e.g. controlled by a voltage  $v \rightarrow u$
- ▶ sensed signals: the distance *d* of the ball to the center of the beam, the angular position  $\theta$  and velocity  $\dot{\theta}$  of the shaft of the motor  $\rightarrow y = [r d, \theta, \dot{\theta}]^T$

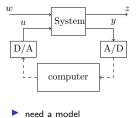
Signals for the control problem:

- tracking objective  $\rightarrow z = r d$
- only exogenous input w = r

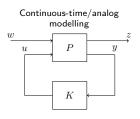
The *performance channel*  $T_{w \to z}$  describes how fast the system will follow the reference. It can be filtered, e.g. with a low-pass filter.

# Fifty shades of models

"Real world"

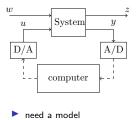


# Fifty shades of models

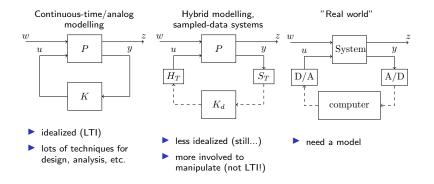


- idealized (LTI)
- lots of techniques for design, analysis, etc.

"Real world"

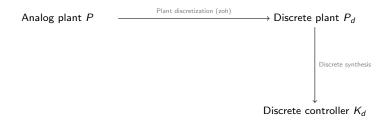


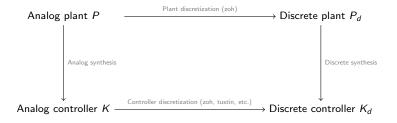
# Fifty shades of models

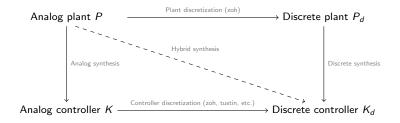


Analog plant P

Discrete controller  $K_d$ 







- indirect methods loose optimality
- intersample behaviour is discarded
- ▶ decreasing *T* requires higher computational power and accuracy  $\hookrightarrow$  with shift operator,  $\lim_{T\to 0} A_d = I$  and  $\lim_{T\to 0} B_d = 0$

# Outline

Performances of a controlled system

Quantifying discretization error

Continuous lifting and measure of performance for SD systems

Conclusion

## Ideal sampler & holder

Reminder: LTI model G, i/o relationship in frequency domain

analog:  $Y(j\omega) = G_a(j\omega)U(j\omega)$  discrete:  $Y(e^{j\omega}) = G_d(e^{j\omega})U(e^{j\omega})$ 

## Ideal sampler & holder

Reminder: LTI model G, i/o relationship in frequency domain

analog:  $Y(j\omega) = G_a(j\omega)U(j\omega)$  discrete:  $Y(e^{j\omega}) = G_d(e^{j\omega})U(e^{j\omega})$ Sampler  $S_T$ 

$$\xrightarrow{V}$$
  $S_T \rightarrow \xrightarrow{V_s}$ 

- time domain:  $v_s[k] = v(kT)$
- modelled by an impulse-train  $\sum_k \delta(t kT) = T$ -periodic function
- ▶ frequency domain:  $V_s(e^{-j\omega T}) = \frac{1}{T} \sum_{k \in \mathbb{Z}} V(j\omega + jk\omega_s)$  frequency aliasing
- /!\not bounded for all signals in L<sub>2</sub> (bandlimited signals or anti-aliasing filter)

## Ideal sampler & holder

Reminder: LTI model G, i/o relationship in frequency domain

analog:  $Y(j\omega) = G_a(j\omega)U(j\omega)$  discrete:  $Y(e^{j\omega}) = G_d(e^{j\omega})U(e^{j\omega})$ Sampler  $S_T$ 

$$\xrightarrow{V}$$
  $S_T \rightarrow \xrightarrow{V_s}$ 

• time domain: 
$$v_s[k] = v(kT)$$

- modelled by an impulse-train  $\sum_k \delta(t kT) = T$ -periodic function
- ▶ frequency domain:  $V_s(e^{-j\omega T}) = \frac{1}{T} \sum_{k \in \mathbb{Z}} V(j\omega + jk\omega_s)$  frequency aliasing

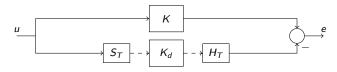
▶ /!\not bounded for all signals in  $\mathcal{L}_2$  (bandlimited signals or anti-aliasing filter) Holder  $H_T$ 

$$V_{s} \rightarrow H_{T} \rightarrow V_{s}$$

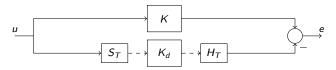
- time domain:  $v(t) = v_s[k]$ ,  $kT \le t < (k+1)T$
- modelled as a difference of delayed steps:  $h_T(t) = \frac{1}{T}\mathbf{1}(t) \frac{1}{T}\mathbf{1}(t-T)$
- Frequency domain:  $H_T(s) = \frac{1-e^{-sT}}{sT}$  and  $V(j\omega) = TH_T(j\omega)V_s(e^{-j\omega T})$

Let K be an analog LTI model and  $K_d$  its discretization: Meaningful notion of error?

Let K be an analog LTI model and  $K_d$  its discretization: Meaningful notion of error?



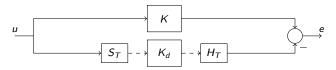
Let K be an analog LTI model and  $K_d$  its discretization: Meaningful notion of error?



- the error system is time-varying (*T*-periodic)  $\rightarrow$  no transfer function
- ▶  $H_T S_T$  is not bounded for all signals in  $\mathcal{L}_2 \rightarrow$  need bandlimited signal *u* or anti-aliasing filter
- frequency-domain error:

$$E(j\omega) = K(j\omega)U(j\omega) - H_T(j\omega)K_d(e^{-j\omega T})\sum_k U(j\omega + jk\omega_s)$$
(2)

Let K be an analog LTI model and  $K_d$  its discretization: Meaningful notion of error?



- the error system is time-varying (*T*-periodic)  $\rightarrow$  no transfer function
- ▶  $H_T S_T$  is not bounded for all signals in  $\mathcal{L}_2 \rightarrow$  need bandlimited signal *u* or anti-aliasing filter
- frequency-domain error:

$$E(j\omega) = K(j\omega)U(j\omega) - H_T(j\omega)K_d(e^{-j\omega T})\sum_k U(j\omega + jk\omega_s)$$
(2)

suppose  $U(j\omega) = 0$  for  $\omega > \omega_N$  (bandlimited),

$$E(j\omega) = \left(K(j\omega) - H_T(j\omega)K_d(e^{-j\omega T})\right)U(j\omega)$$
(3)

 $\rightarrow error(\omega) = \left| K(j\omega) - H_T(j\omega) K_d(e^{-j\omega T}) \right|$ 

# Discretization error: example

$$K(s) = \frac{1}{1 + 0.7s/10 + s^2/100} \tag{4}$$

$$T_1 = 0.01 \rightarrow K_d^1$$

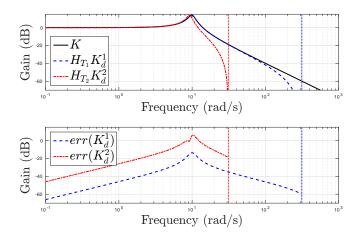
$$T_2 = 0.1 \rightarrow K_d^2$$

# Discretization error: example

$$K(s) = \frac{1}{1 + 0.7s/10 + s^2/100}$$
(4)

$$T_1 = 0.01 \rightarrow K_d^1$$

$$T_2 = 0.1 \rightarrow K_d^2$$

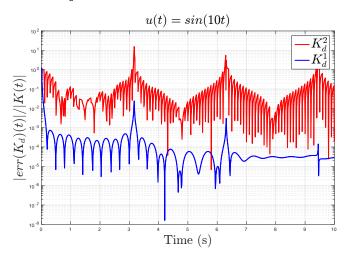


## Discretization error: example

$$K(s) = \frac{1}{1 + 0.7s/10 + s^2/100}$$
<sup>(4)</sup>

$$T_1 = 0.01 \rightarrow K_d^1$$

$$T_2 = 0.1 \rightarrow K_d^2$$



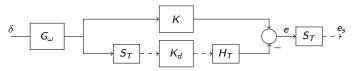
# Optimal discretization?

- frequency-domain error not usual system norm
- possible to look for the best discretization scheme w.r.t. the sampling instants and w.r.t. a predefined class of signals

 $\hookrightarrow$ section 4.6 in [2]

 $\hookrightarrow$ usual discrete norm can be used to measure  $e_s$ 

 $\hookrightarrow$ e.g. step invariant discretization (ZOH) is the solution for steps



<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

# Outline

Performances of a controlled system

Quantifying discretization error

Continuous lifting and measure of performance for SD systems

Conclusion

# Lifting continuous signals

Frequency-domain considerations are central in some design methods...but SD have no transfer function

# Lifting continuous signals

# Frequency-domain considerations are central in some design methods...but SD have no transfer function

#### **Continuous lifting**

Consider a signal u(t) such that  $\int_{-\infty}^{\infty} u(t)^2 dt < \infty$  (i.e.  $\in \mathcal{L}_2(\mathbb{R})$ )

1. divide u in chunks of length T (sampling time): ..., [-T, 0), [0, T), [T, 2T), ...

# Lifting continuous signals

# Frequency-domain considerations are central in some design methods...but SD have no transfer function

#### **Continuous lifting**

Consider a signal u(t) such that  $\int_{-\infty}^{\infty} u(t)^2 dt < \infty$  (i.e.  $\in \mathcal{L}_2(\mathbb{R})$ )

- 1. divide u in chunks of length T (sampling time): ..., [-T, 0), [0, T), [T, 2T), ...
- 2. call the k-th chunk  $u_k$  such that  $u_k(t) = u(kT + t)$  for  $0 \le t < T$

# Lifting continuous signals

# Frequency-domain considerations are central in some design methods...but SD have no transfer function

#### **Continuous lifting**

Consider a signal u(t) such that  $\int_{-\infty}^{\infty} u(t)^2 dt < \infty$  (i.e.  $\in \mathcal{L}_2(\mathbb{R})$ )

- 1. divide u in chunks of length T (sampling time): ..., [-T, 0), [0, T), [T, 2T), ...
- 2. call the k-th chunk  $u_k$  such that  $u_k(t) = u(kT + t)$  for  $0 \le t < T$
- 3. introduce the discrete-time signal  $\underline{u} = \{u_k\}_k$

# Lifting continuous signals

# Frequency-domain considerations are central in some design methods...but SD have no transfer function

#### **Continuous lifting**

Consider a signal u(t) such that  $\int_{-\infty}^{\infty} u(t)^2 dt < \infty$  (i.e.  $\in \mathcal{L}_2(\mathbb{R})$ )

- 1. divide u in chunks of length T (sampling time): ..., [-T, 0), [0, T), [T, 2T), ...
- 2. call the k-th chunk  $u_k$  such that  $u_k(t) = u(kT + t)$  for  $0 \le t < T$
- 3. introduce the discrete-time signal  $\underline{u} = \{u_k\}_k$
- 4. <u>u</u> lies in  $l_2(\mathbb{Z}, \mathcal{K})$  where  $\mathcal{K} = \mathcal{L}_2([0, T))$

# Lifting continuous signals

# Frequency-domain considerations are central in some design methods...but SD have no transfer function

#### **Continuous lifting**

Consider a signal u(t) such that  $\int_{-\infty}^{\infty} u(t)^2 dt < \infty$  (i.e.  $\in \mathcal{L}_2(\mathbb{R})$ )

- 1. divide u in chunks of length T (sampling time): ..., [-T, 0), [0, T), [T, 2T), ...
- 2. call the k-th chunk  $u_k$  such that  $u_k(t) = u(kT + t)$  for  $0 \le t < T$
- 3. introduce the discrete-time signal  $\underline{u} = \{u_k\}_k$
- 4. <u>u</u> lies in  $l_2(\mathbb{Z}, \mathcal{K})$  where  $\mathcal{K} = \mathcal{L}_2([0, T))$

Lifting operator:

$$\begin{array}{rcl} L: & \mathcal{L}_2(\mathbb{R}) & \to & h_2(\mathbb{Z}, \mathcal{K}) \\ & u(t) & \to & \underline{u} \end{array}$$
 (5)

#### ▶ it turns out L is an isomorphism →working with u or u is 'equivalent'

$$G: \begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases} \text{ such that } y = Gu$$
(6)

>

Lifted system  $\underline{G}$  obtained by lifting input/output

• 
$$\underline{u} = Lu$$
  
•  $\underline{y} = Ly$   
• thus  $\underline{y} = \underline{Gu}$  with  $\underline{G} = LGL^{-1}$   
 $- \rightarrow L^{-1}$ 

$$\xrightarrow{L^{-1}} G \xrightarrow{L^{-1}} G$$

$$G: \begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases} \text{ such that } y = Gu$$
(6)

Lifted system  $\underline{G}$  obtained by lifting input/output

• 
$$\underline{u} = Lu$$
  
•  $\underline{y} = Ly$   
• thus  $\underline{y} = \underline{Gu}$  with  $\underline{G} = LGL^{-1}$   
•  $- \rightarrow \underbrace{L^{-1}}_{\underline{G}} \xrightarrow{G} L^{-} \rightarrow \underbrace{G}_{\underline{G}}$ 

 $\underline{\mathsf{G}}$  represented by discrete-time equations

$$\underline{\mathbf{G}}: \begin{cases} \xi_{k+1} = \underline{\mathbf{A}}\xi_k + \underline{\mathbf{B}}u_k \\ y_k = \underline{\mathbf{C}}\xi_k + \underline{\mathbf{D}}u_k \end{cases} \quad \text{with} \quad \xi_k = \mathbf{x}(kT)$$
(7)

$$G: \begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases} \text{ such that } y = Gu$$
(6)

Lifted system  $\underline{G}$  obtained by lifting input/output

$$\underline{u} = Lu$$

$$\underline{y} = Ly$$

$$thus \underline{y} = \underline{Gu} \text{ with } \underline{G} = LGL^{-1}$$

$$- \cancel{L^{-1}} \xrightarrow{G} \underbrace{L^{-1}}_{G} \xrightarrow{L^{-1}}_{G} \xrightarrow{L^{-1}}_{G} \xrightarrow{L^{-1}}_{G} \xrightarrow{L^{-1}}_{G} \xrightarrow{L^{-1}}_{G} \xrightarrow{L^$$

 $\underline{G}$  represented by discrete-time equations

$$\underline{\mathbf{G}}: \begin{cases} \xi_{k+1} = \underline{\mathbf{A}}\xi_k + \underline{\mathbf{B}}u_k \\ y_k = \underline{\mathbf{C}}\xi_k + \underline{\mathbf{D}}u_k \end{cases} \quad \text{with} \quad \xi_k = \mathbf{x}(kT)$$
(7)

where the transformations are

$$\underline{A}: \quad \mathcal{E} \to \mathcal{E}, \quad \underline{A}\xi = e^{TA}\xi \\
\underline{B}: \quad \mathcal{K} \to \mathcal{E}, \quad \underline{B}u = \int_{0}^{T} e^{(T-\tau)A} Bu(\tau) d\tau \\
\underline{C}: \quad \mathcal{E} \to \mathcal{K}, \quad (\underline{C}\xi)(t) = Ce^{tA}\xi \\
\underline{D}: \quad \mathcal{K} \to \mathcal{K}, \quad (\underline{D}u)(t) = Du(t) + \int_{0}^{t} Ce^{(t-\tau)A} Bu(\tau) d\tau$$
(8)

Interest?

- $D_T$  and  $D_T^*$ : time delay and time advance of T
- U and U\*: unit time delay and advance on  $I_2(\mathbb{Z},\mathcal{K})$

Interest?

- $D_T$  and  $D_T^*$ : time delay and time advance of T
- ► U and U\*: unit time delay and advance on l<sub>2</sub>(Z, K)

Note that time-delays translate to shifts in the lifted domain:

$$LD_T^* = U^*L$$
 and  $L^{-1}U = D_T L^{-1}$  (9)

Interest?

- $D_T$  and  $D_T^*$ : time delay and time advance of T
- U and U\*: unit time delay and advance on  $I_2(\mathbb{Z},\mathcal{K})$

Note that time-delays translate to shifts in the lifted domain:

$$LD_T^* = U^*L \text{ and } L^{-1}U = D_T L^{-1}$$
(9)

*G* is *T*-periodic  $\Leftrightarrow \underline{G}$  is time invariant

Proof  $(\Rightarrow)$ 

$$U^* \underline{G} U = U^* L G L^{-1} U$$
  
=  $L D_T^* G D_T L^{-1}$   
=  $L G L^{-1}$   
 $\triangleq \underline{G}$  (10)

Interest?

- $D_T$  and  $D_T^*$ : time delay and time advance of T
- U and U<sup>\*</sup>: unit time delay and advance on  $l_2(\mathbb{Z}, \mathcal{K})$

Note that time-delays translate to shifts in the lifted domain:

$$LD_T^* = U^*L$$
 and  $L^{-1}U = D_T L^{-1}$  (9)

*G* is *T*-periodic  $\Leftrightarrow \underline{G}$  is time invariant

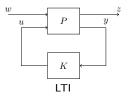
Proof  $(\Rightarrow)$ 

$$U^* \underline{G} U = U^* L G L^{-1} U$$
  
=  $L D_T^* G D_T L^{-1}$   
=  $L G L^{-1}$   
 $\triangleq \underline{G}$  (10)

A SD system can be lifted into a time-invariant discrete-time system with infinite-dimensional input and output spaces

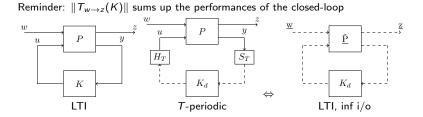
# Measure of performance of closed-loop SD systems I

Reminder:  $||T_{w\to z}(K)||$  sums up the performances of the closed-loop



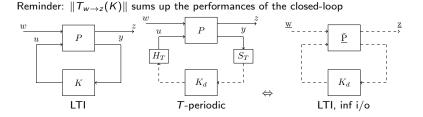
<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

### Measure of performance of closed-loop SD systems I



<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

## Measure of performance of closed-loop SD systems I



In chap. 12-13 of [2]:

- ▶ similar norms (2 and  $\infty$ ) can be defined for  $T_{w \to z}(K_d)$  through  $T_{\underline{W} \to \underline{z}}(K_d)$
- …leading to some optimal synthesis framework
- …and analysis
- but more difficult due to infinite dimensionality of input/output spaces

<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

# Measure of performance of closed-loop SD systems II

### Some interesting applications in [2]

Consider two discretizations  $K_d^1(T)$  and  $K_d^2(T)$  of some controller K

- compare their performances against sampling rate T → example 13.7.3
- ▶ determine  $T_{max}$  such that some prescribed performance bound is fulfilled  $\hookrightarrow$  example 13.8.1
- ▶ perform optimal synthesis in SD framework ↔ example 13.8.1

<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

# Measure of performance of closed-loop SD systems II

### Some interesting applications in [2]

Consider two discretizations  $K_d^1(T)$  and  $K_d^2(T)$  of some controller K

- compare their performances against sampling rate T → example 13.7.3
- ▶ determine  $T_{max}$  such that some prescribed performance bound is fulfilled  $\hookrightarrow$  example 13.8.1
- ▶ perform optimal synthesis in SD framework ↔ example 13.8.1

#### Other?

• given P, K, for fixed T, find  $K_d$  that minimizes the loss of performance w.r.t. analog design

$$\|T_{\underline{W}\to\underline{Z}}(K) - T_{\underline{W}\to\underline{Z}}(K_d)\|$$
(11)

 $\hookrightarrow$  everything must be considered in the lifted domain

<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

# Outline

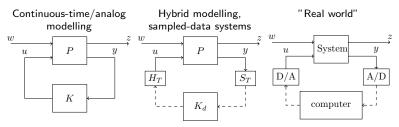
Performances of a controlled system

Quantifying discretization error

Continuous lifting and measure of performance for SD systems

Conclusion

# Conclusion



- Sampled-Data formalism suited for computer-controlled systems
- Lifting technique to extend LTI tools
- Lifting can also be used to handle multiple sampling rates, chap. 8 [2]
- infinite dimensionality...
- still not implemented controller (code)...

Tools: [3], [4]

<sup>[2]</sup> Chen and Francis. Optimal sampled-data control systems. 1995

<sup>[3]</sup> Fujioka, Hara, and Yamamoto. "Sampled-data control toolbox: object-oriented software for sampled-data feedback control systems". 2004

<sup>[4]</sup> Polyakov, Rosenwasser, and Lampe. "DIRECTSD 3.0 toolbox for MATLAB: Further progress in polynomial design of sampled-data systems". 2006

# References I

F

S. Boyd and C. Barratt. *Linear controller design: limits of performance*. Prentice Hall Englewood Cliffs, NJ, 1991.

T. Chen and B.A. Francis. *Optimal sampled-data control systems*. Springer Science & Business Media, 1995.

H. Fujioka, S. Hara, and Y. Yamamoto. "Sampled-data control toolbox: object-oriented software for sampled-data feedback control systems". In: *International Conference on Robotics and Automation*. 2004, pp. 19–24.

K. Polyakov, E. Rosenwasser, and B. Lampe. "DIRECTSD 3.0 toolbox for MATLAB: Further progress in polynomial design of sampled-data systems". In: *Conference on Computer Aided Control System Design*. 2006, pp. 1946–1951.